Journal of King Saud University - Science 36 (2024) 103545

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Journal of King Saud University - Science

journal homepage: www.sciencedirect.com

Full Length Article

The influence of pathological conditions on vocal cord's displacement: A numerical method and data analysis

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ARTICLE INFO

Keywords:
Displacements of vocal cords
Cubic trigonometric B-spline
One-mass model of vocal cord

ABSTRACT

In this study, one-mass model of vocal cord is solved by using cubic trigonometric B-spline (CTBS) in order to generate displacements of healthy and pathological vocal cord. By utilizing CTBS, this work aims to investigate the relationship between five vocal cord conditions and its displacements generation throughout phonation process. The approximate displacements derived from CTBS are then compared to displacement generated by ode45 built-in solver through MATLAB software. The errors from both methods are then calculated which represented the effectiveness of the CTBS method in generating vocal cord displacements. Any discrepancies between the results generated by using CTBS and ode45 can be analysed to prove the reliability of CTBS method. Besides, an error analysis is demonstrated in order to quantitatively evaluate the accuracy of the approximate solutions. The generated approximate displacements of CTBS have shown to be approximately close to ode45 results. Thus, it can be concluded that CTBS is a reliable numerical method. The relationship between vocal cord conditions and its generated displacements has represented the distinction between healthy and pathological vocal cord outcomes. Healthy vocal cord has generated a steady decline displacements value while vocal cords with pathological condition have generated fluctuated displacement values throughout the phases of phonation process. The fluctuation trend of displacements value has revealed the irregular displacements value generation which is one of pathological vocal cord feature caused by low stiffness.

1. Introduction

Speech production involves a complex interplay of physiological processes, with the vocal cords playing a crucial role in sound generation. The vocal cords, also known as vocal folds, are essential components of the larynx responsible for producing voice sounds. The vocal cords vibrate as the air passes through the larynx from lungs, which then form the basis of speech created by the sound waves. The larynx, also known as the voice box, is a structure located at the top of the trachea that involved in sound production process, breathing, and swallowing. The larynx contains the vocal cords, which are fold-like soft tissue that vibrates to produce sound. The distance between the opening of vocal cords is called glottis, that function to opens and closes, during breathing, swallowing and sound production process. Lot of researches have been conducted to study the movements of vocal cord through experiment and mathematical modelling approach.

The evolution of mechanical models of vocal cords has progressed from the basic one-mass model (Flanagan and Landgraf, 1968) to more complex multi-mass models (Drioli and Aichinger, 2021), as discussed in various research papers. Initially, the one-mass nonlinear oscillator system was accepted as the fundamental model for describing voice production. Over time, this model has been extended into three (Story and Titze, 1993), five (Yang et al., 2010), and more mass systems, incorporating time variable parameters (Cveticanin, 2015) and three-dimensional aspects (Lan, 2006), as well as simplified into systems with coupled deflection (Zheng et al., 2011) and damping functions (Fulcher et al., 2006). These advancements have allowed for more detailed description of the vibrations of symmetric (Tao et al., 2007) and asymmetric vocal cords (Erath et al., 2019), providing insights into regular and irregular motions like bifurcation (Mehdi and Mohammad, 2019) and deterministic chaos (Jiang and Zhang, 2002) in vocal cords. The progression from simpler one-mass models to more intricate multi-mass systems has significantly enhanced our understanding of the mechanical behaviour of vocal cords and their role in voice production.

The one-mass model of vocal cords by Flanagan is a significant advancement in vocal cord modelling, particularly in understanding the

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https://doi.org/10.1016/j.jksus.2024.103545
Received 16 August 2024; Received in revised form 4 November 2024; Accepted 14 November 2024
Available online 16 November 2024

Table 1
Parameters used in solving Eq. (1) (Cataldo et al., 2006; Flanagan and Landgraf, 1968).

Parameter	Value
m	0.240×10^{-3} kg
b	0.667 Ns/m
k	4.925×10^{5} Ns/m
t	0.050 s
P_s	783 Pa
ρ	1.300×10^{3} kg/m^3
l	1.800×10^{-2} m
d	0.300×10^{-3} m
h	1.000×10^{-4}

Table 2
Average fundamental frequencies of healthy and pathological conditions of vocal cords.

Vocal cord conditions	Fundamental frequency, f_0 (Hz)
Healthy	453.7542
Hyperfunctional dysphonia	426.1522
Laryngitis	383.8566
Functional dysphonia	433.9783
Recurrent laryngeal nerve paralysis	418.1722

nonlinear interaction between vocal cord displacement and airflow. This model describes the system's behaviour qualitatively similar to higher-dimensional models like the two-mass Ishizaka-Flanagan model (Ishizaka and Flanagan, 1972), showcasing its effectiveness in capturing essential dynamics of vocal cord vibration (Mcgowan and Howe, 2010). The one-mass model simplifies the complex mechanics of vocal cord oscillation into a more manageable framework, aiding in the study of voice production and pathology detection (Perrine et al., 2020). By incorporating the one-mass model, researchers can simulate vocal cord vibrations accurately and efficiently, enhancing the understanding of vocal physiology and potential disorders. Further, this work aims to generate displacements of vocal cord by solving one-mass model of vocal cord.

Numerical methods play an important role in solving various problems (Abd El-Hady & El-shenawy, 2024; Shirokova & El-Shenawy, 2018) such as mechanical models, (El-shenawy, El-Gamel, & Teba, 2024) and also to solve mechanical model of vocal cords. A numerical model called simVoice is introduced, which includes experimentally obtained vocal cord motion to simplify computational expenses and enhance efficiency (Maurerlehner et al., 2021). The numerical simulation of vocal cord vibrations excited by compressible viscous flow for flow and elasticity problems which involves space–time discontinuous Galerkin method and the backward difference formula in time and discontinuous Galerkin method in space (Balázsová et al., 2021). Furthermore, the mathematical model and numerical simulation of flow-induced vibrations of human vocal cords model employ the finite element method with SUPG and PSPG stabilization methods for fluid flow approximation, emphasizing the importance of inlet boundary conditions (Sváček and Horáček, 2018). Lastly, a study on vocal cord asymmetric collision presents a position-based contact model with variational methods for contact enforcement and highlights the impact of contact on vocal cord dynamics and oscillations (Granados et al., 2017).

The B-spline collocation method is a powerful numerical technique used in solving both initial value problems (IVPs) (Islam, 2015) and boundary value problems (BVPs) (Goh et al., 2012) efficiently. Various studies have highlighted the effectiveness of this method in providing accurate approximations for a wide range of problems. For instance, the uniform cubic B-spline collocation method has been successfully applied to linear (Goh, 2013) and nonlinear fractional IVPs (Rabah et al., 2022), demonstrating its validity and applicability (Tayebi et al., 2022). Additionally, the quintic B-spline collocation method has shown fourth-order convergence results when solving non-linear BVPs, showcasing its proficiency in handling such problems (Tok Onarcan et al., 2023). Moreover, the orthogonal cubic spline collocation technique has been utilized for two-point interface BVPs, emphasizing its computational superiority and stability over other methods (Bhal and Panda, 2022). There are few types of B-spline basis function such as B-spline, trigonometric B-spline (Chawla et al., 2023; Yaseen et al., 2017) and hybrid B-spline (Zin, 2016) that has widely used to solve various mathematical problems.

Since one-mass model of vocal cord is an initial value problem, cubic trigonometric B-spline (CTBS) (El-El-shenawy et al., 2024b) is chosen to solve this model and generate approximate displacements of vocal cord. Besides, CTBS is a simple and straightforward (Abbas et al., 2014) method to generate displacements of vocal cord. Abbas et al. state that the benefit of employing the suggested method is that, compared to the finite difference approach, which only provides the solution at specific points, it generates a spline function on each new time line that can be

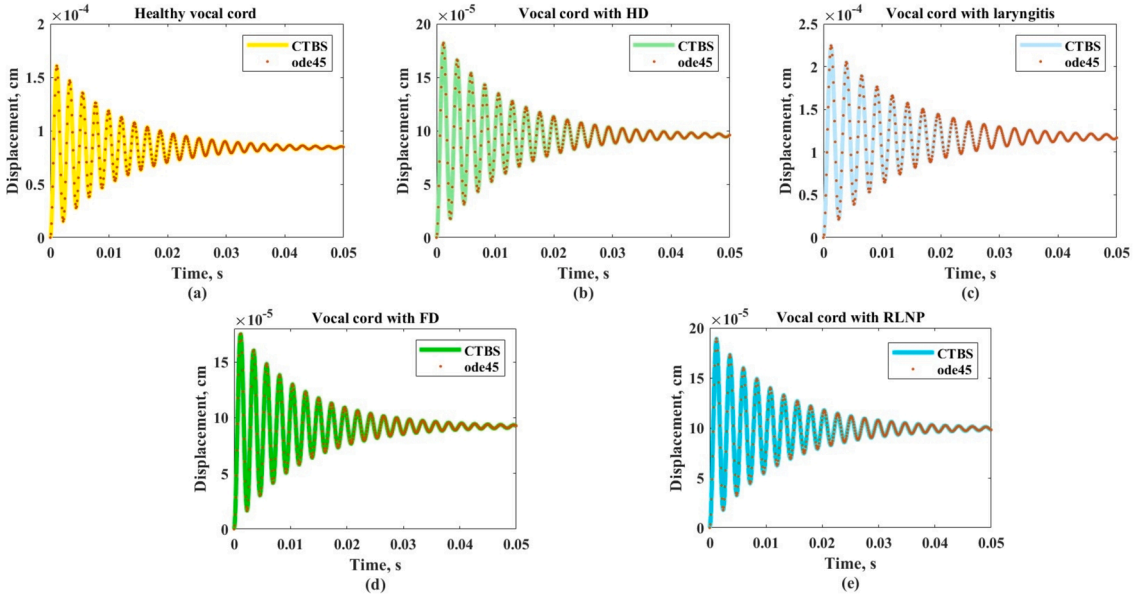

Fig. 1. Displacements of (a) healthy vocal cord, vocal cord with (b) HD, (c) laryngitis, (d) FD and (e) RLNP generated by using CTBS and ode45 within 0.05 s.

Table 3
Displacements of each vocal cords condition obtained by using CTBS and ode4 within 0.05 s.

Time (s)	Displacements (cm)									
	Healthy		HD		Laryngitis		FD		RLNP	
	CTBS	ode45	CTBS	ode45	CTBS	ode45	CTBS	ode45	CTBS	ode45
0.010	1.1878×10^{-4}	1.1847×10^{-4}	9.3446×10^{-5}	9.2517×10^{-5}	9.3431×10^{-5}	9.5274×10^{-5}	1.0876×10^{-4}	1.0790×10^{-4}	1.0876×10^{-4}	1.0790×10^{-4}
0.015	8.0780×10^{-5}	8.1291×10^{-5}	1.1362×10^{-4}	1.1269×10^{-4}	1.2106×10^{-4}	1.2295×10^{-4}	1.1767×10^{-4}	1.1724×10^{-4}	1.1767×10^{-4}	1.1724×10^{-4}
0.020	7.0404×10^{-5}	7.0602×10^{-5}	1.1345×10^{-4}	1.1308×10^{-4}	1.3308×10^{-4}	1.3429×10^{-4}	1.0253×10^{-4}	1.0288×10^{-4}	1.0253×10^{-4}	1.0288×10^{-4}
0.025	8.6857×10^{-5}	8.6491×10^{-5}	1.0455×10^{-4}	1.0479×10^{-4}	1.3420×10^{-4}	1.3449×10^{-4}	8.8370×10^{-5}	8.8979×10^{-5}	8.8370×10^{-5}	8.8979×10^{-5}
0.030	8.9785×10^{-5}	8.9697×10^{-5}	9.6264×10^{-5}	9.6773×10^{-5}	1.2988×10^{-4}	1.2994×10^{-4}	8.5128×10^{-5}	8.5408×10^{-5}	8.5128×10^{-5}	8.5408×10^{-5}
0.035	8.2788×10^{-5}	8.3004×10^{-5}	9.2327×10^{-5}	9.2744×10^{-5}	1.2427×10^{-4}	1.2348×10^{-4}	8.8951×10^{-5}	8.8813×10^{-5}	8.8951×10^{-5}	8.8813×10^{-5}
0.040	8.2152×10^{-5}	8.2182×10^{-5}	9.2217×10^{-5}	9.2373×10^{-5}	1.1972×10^{-4}	1.1894×10^{-4}	9.2952×10^{-5}	9.2685×10^{-5}	9.2952×10^{-5}	9.2685×10^{-5}
0.045	8.5079×10^{-5}	8.4962×10^{-5}	9.3819×10^{-5}	9.3753×10^{-5}	1.1701×10^{-4}	1.1646×10^{-4}	9.4061×10^{-5}	9.3929×10^{-5}	9.4061×10^{-5}	9.3929×10^{-5}
0.050	8.5102×10^{-5}	8.5097×10^{-5}	9.5372×10^{-5}	9.5219×10^{-5}	1.1596×10^{-4}	1.1571×10^{-4}	9.3113×10^{-5}	9.3154×10^{-5}	9.3113×10^{-5}	9.3154×10^{-5}

Table 4
Errors of each vocal cords condition obtained within 0.05 s.

Time (s)	Errors				
	Healthy	HD	Laryngitis	FD	RLNP
0.010	3.0474×10^{-7}	9.2841×10^{-7}	1.8423×10^{-6}	8.6056×10^{-7}	8.6056×10^{-7}
0.015	5.1106×10^{-7}	9.2687×10^{-7}	1.8877×10^{-6}	4.2781×10^{-7}	4.2781×10^{-7}
0.020	1.9810×10^{-7}	3.6930×10^{-7}	1.2091×10^{-6}	3.4659×10^{-7}	3.4659×10^{-7}
0.025	3.6570×10^{-7}	2.4035×10^{-7}	2.9217×10^{-7}	6.0949×10^{-7}	6.0949×10^{-7}
0.030	8.8213×10^{-8}	5.0958×10^{-7}	4.3992×10^{-7}	2.8026×10^{-7}	2.8026×10^{-7}
0.035	2.1665×10^{-7}	4.1664×10^{-7}	7.8928×10^{-7}	1.3728×10^{-7}	1.3728×10^{-7}
0.040	2.9324×10^{-8}	1.5561×10^{-7}	7.7928×10^{-7}	2.6748×10^{-7}	2.6748×10^{-7}
0.045	1.1605×10^{-7}	6.5709×10^{-8}	5.4700×10^{-7}	1.3223×10^{-7}	1.3223×10^{-7}
0.050	5.1934×10^{-9}	1.5306×10^{-7}	2.5222×10^{-7}	4.0653×10^{-8}	4.0653×10^{-8}

Table 5
Displacements generated by each condition throughout phonation process.

Conditions	Displacements throughout phonation process (cm)		
	Early phase, 0.010 s	Middle phase, 0.030 s	End phase, 0.050 s
Healthy	1.1878×10^{-4}	8.9785×10^{-5}	8.5102×10^{-5}
HD	9.3446×10^{-5}	9.6264×10^{-5}	9.5372×10^{-5}
Laryngitis	9.3431×10^{-5}	1.2988×10^{-4}	1.1596×10^{-4}
FD	1.0876×10^{-4}	8.5128×10^{-5}	9.3113×10^{-5}
RLNP	7.6495×10^{-5}	1.0769×10^{-4}	9.8421×10^{-5}

utilized to get the solutions of any intermediate point in the space direction. Subsequently, in order to prove the reliability of the proposed method, the error obtained by the proposed method will be calculated by comparing the generated displacements to ode45. Ode45 is a built-in solver through MATLAB software that has been widely used to solve various problems (Anyigor & Afiukwa, 2013; Postawa et al., 2020).

In conclusion, this study will generate the approximate displacements of one-mass model for healthy and pathological vocal cord using CTBS and verified by the ode45. Any discrepancies between both results can be analysed and proved the reliability of CTBS method. Besides, an

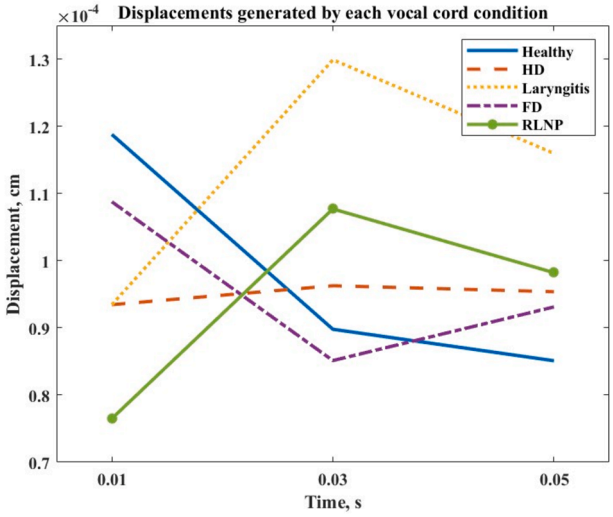

Fig. 2. Displacements generated by each vocal cord conditions throughout the phases of phonation process.

error analysis is done in order to quantitatively evaluate the accuracy of the approximate solutions. This study will also investigate the relationship between vocal cord conditions and its displacements generation throughout phonation process.

2. Parameters

In this work, one-mass mechanical model of vocal cord is solved to generate displacements of vocal cord. The equation of the model is given by (Flanagan and Landgraf, 1968)

$$mx''(t) + bx'(t) + kx(t) = F(t), \tag{1}$$

with the following initial conditions

$$x(t_0) = \alpha \text{ and } x'(t_0) = \beta, \tag{2}$$

where $x(t)$ is displacement of vocal cord, m is mass, b is damping, k is spring constant while $F(t)$ is forcing function. The value of mass, damping and spring constant can be calculated by

$$mass,\quad m=\frac{1}{4}\sigma l^2 d, \tag{3}$$

$$damping,\quad b=2\sqrt{mk}, \tag{4}$$

and

$$springconstant,\quad k=4\pi^2 m(f_0)^2, \tag{5}$$

where σ is the density of vocal cord flesh, l is the cord length, d is the vocal cord thickness, and f_0 is fundamental frequency. The forcing function is calculated by $F(t)=\frac{1}{2}(P_1+P_2)(ld)$ where P_1 and P_2 are the acoustic pressures at the inlet and outlet of the glottal orifice, and can be obtained by $P_1=P_s-1.37P_B$ and $P_2=-0.50P_B$. P_s is subglottal pressure and P_B is Bernoulli pressure and can be calculated by $P_B=\frac{1}{2}\rho|U_g|^2Ag^{-2}$ while the value of displacements and fundamental frequencies will be calculated in the next section.

3. Methodology

This section explained methodology in finding fundamental frequencies, f_0 and approximate displacements of five vocal cord conditions. The conditions are healthy, laryngitis, hyperfunctional dysphonia, functional dysphonia and recurrent laryngeal nerve paralysis. Subsection 3.1 discussed the method used to generate fundamental frequency. Then, subsection 3.2 and 3.3 discussed the generation of displacements by using CTBS and ode45 respectively.

3.1. Fundamental frequency

Origin is a data analysis and graphing software that also offered analysis tools and apps for signal processing. The software is used to obtain fundamental frequencies. The fundamental frequencies are obtained by the following steps:

i. 100 voice recordings of each vocal cord conditions are gathered from Saarbruecken Voice Database (Barry and Pützer, 2007).
ii. The recordings are then, imported into Origin, in order to generate the frequencies, providing the magnitude, amplitude, phase, one/two-sided power density, and other computation results.
iii. From the frequency values, fundamental frequencies of the recording can be obtained to find the value of k from Eq. (5) as follows:

$$f_0=\text{Index of the largest power}\times F_s+F0, \tag{6}$$

where the index of the largest power can be obtained from FFT result, f_0 is frequency resolution and $F0$ is the starting frequency value.
iv. Further, the average fundamental frequency of each condition is calculated and used in proposed method.

3.2. Cubic trigonometric B-spline (CTBS)

This subsection discusses CTBS method in generating approximate displacements of vocal cord by solving Eq. (1). In CTBS, the knot with non-decreasing sequence is considered as $\{t_0,t_1,\ldots t_{j-1},t_j,t_{j+1},\ldots t_n\}$ where $t_{j-1}\leqslant t_j\leqslant t_{j+1}$ for $j=0,1,\ldots n$. The $j-$th basis of trigonometric B-spline, $T_j^k(t)$ of order k can be calculated using (Walz, 1997)

$$T_j^k(t)=\frac{\sin\left(\frac{t-t_j}{2}\right)}{\sin\left(\frac{t_{j+k-1}-t_j}{2}\right)}T_j^{k-1}(t)+\frac{\sin\left(\frac{t_{j+k}-t}{2}\right)}{\sin\left(\frac{t_{j+k}-t_{j+1}}{2}\right)}T_{j+1}^{k-1}(t), \tag{7}$$

where CTBS basis of order one is defined as

$$T_j^1(t)=\begin{cases}1, & t\in[t_j,t_{j+1}],\\ 0, & \text{otherwise.}\end{cases} \tag{8}$$

Then, the CTBS basis of order four is defined as

$$T_j^4(t)=\frac{1}{\theta}\begin{cases}\sigma^3(t_j), & t\in[t_j,t_{j+1}],\\ \sigma(t_j)\left[\sigma(t_j)\varsigma(t_{j+2})+\varsigma(t_{j+3})\sigma^2(t_{j+1})\right] & \\ \quad+\varsigma(t_{j+4})\sigma^2(t_{j+1}), & t\in[t_{j+1},t_{j+2}],\\ \sigma(t_j)\varsigma^2(t_{j+3})+\varsigma(t_{j+4}) & \\ \left[\sigma(t_{j+1})\varsigma(t_{j+3})+\varsigma(t_{j+4})\sigma(t_{j+2})\right], & t\in[t_{j+2},t_{j+3}],\\ \varsigma^3(t_{j+4}), & t\in[t_{j+3},t_{j+4}],\\ 0, & \text{otherwise,}\end{cases} \tag{9}$$

where $\sigma(t_j)=\sin\left(\frac{t-t_j}{2}\right),\varsigma(t_j)=\left(\frac{t_j-t}{2}\right)$ and $\theta=\sin^2\left(\frac{h}{2}\right)\csc(h)\csc\left(\frac{3h}{2}\right)$.

CTBS function, $x^*(t)$ is an approximate displacement generated from a linear combination of the CTBS basis, as in

$$x^*(t)=\sum_{j=-3}^{n-1}C_jT_j^4(t), \tag{10}$$

where C_j are unknowns to be evaluated and T_j^4 is CTBS basis and can be simplified to

$$x^*(t_j)=C_{j-3}T_{j-3}^4(t)+C_{j-2}T_{j-2}^4(t)+C_{j-1}T_{j-1}^4(t)+C_jT_j^4(t), \tag{11}$$

$$x^{*\prime}(t_j)=C_{j-3}T_{j-3}^{4\prime}(t)+C_{j-2}T_{j-2}^{4\prime}(t)+C_{j-1}T_{j-1}^{4\prime}(t)+C_jT_j^{4\prime}(t), \tag{12}$$

$$x^{*\prime\prime}(t_j)=C_{j-3}T_{j-3}^{4\prime\prime}(t)+C_{j-2}T_{j-2}^{4\prime\prime}(t)+C_{j-1}T_{j-1}^{4\prime\prime}(t)+C_jT_j^{4\prime\prime}(t), \tag{13}$$

Three nonzero basis functions of $T_{j-3}^4(t_j),T_{j-2}^4(t_j)$ and $T_{j-1}^4(t_j)$ are included over $[t_j,t_{j+1}]$ subinterval. By considering the nonzero basis functions, Eq. (11) and its derivatives can be simplified and returned as

$$\begin{aligned}x^*(t_j)&=\varsigma_1C_{j-3}+\varsigma_2C_{j-2}+\varsigma_1C_{j-1},\\ x^{*\prime}(t_j)&=-\varsigma_3C_{j-3}+\varsigma_3C_{j-1},\\ x^{*\prime\prime}(t_j)&=\varsigma_4C_{j-3}+\varsigma_5C_{j-2}+\varsigma_4C_{j-1}\end{aligned} \tag{14}$$

with $\varsigma_1=\sin^2\left(\frac{h}{2}\right)\csc(h)\csc\left(\frac{3h}{2}\right)$, $\varsigma_2=\frac{2}{1+2\cos(h)}$, $\varsigma_3=-\frac{3}{4}\csc\left(\frac{3h}{2}\right)$, $\varsigma_4=\frac{3(1+3\cos(h))\csc^2\left(\frac{h}{2}\right)}{16\left(2\cos\left(\frac{h}{2}\right)+\cos\left(\frac{3h}{2}\right)\right)}$, and $\varsigma_5=-\frac{3\cot^2\left(\frac{h}{2}\right)}{2+4\cos(h)}$.

Eq. (14) is then substituted into the equation to produce a matrix system of order $(n+1)$ equation with $(n+3)$ unknown to solve Eq. (1). Next, two equations are needed in order to generate a unique solution. Subsequently, initial condition which given in Eq. (2) is approximated and represented as

$$\begin{aligned}x^*(t_0)&=\varsigma_1C_{j-3}+\varsigma_2C_{j-2}+\varsigma_1C_{j-1}=\alpha,\\ x^{*\prime}(t_0)&=-\varsigma_3C_{j-3}+\varsigma_3C_{j-1}=\beta.\end{aligned} \tag{15}$$

Eq. (15) is added to the system and become

$$[\boldsymbol{A}]_{(n+3)\times(n+3)}\cdot[\boldsymbol{C}]_{(n+3)\times 1}=[\boldsymbol{R}]_{1\times(n+3)}, \tag{16}$$

where

$$\boldsymbol{A}=\begin{bmatrix} \varsigma_1 & \varsigma_2 & \varsigma_1 & 0 & \cdots & \cdots & \cdots & 0\\ \omega_1 & \omega_2 & \omega_3 & 0 & \cdots & \cdots & \cdots & 0\\ 0 & \omega_1 & \omega_2 & \omega_3 & 0 & \cdots & \cdots & 0\\ \vdots & 0 & \omega_1 & \omega_2 & \omega_3 & 0 & \cdots & 0\\ 0 & \cdots & \ddots & \ddots & \ddots & \cdots & \cdots & 0\\ 0 & \cdots & \cdots & \cdots & 0 & \omega_1 & \omega_2 & \omega_3\\ \varsigma_3 & 0 & \varsigma_3 & 0 & \cdots & \cdots & \cdots & 0 \end{bmatrix},\boldsymbol{C}=\begin{bmatrix} C_{-3}\\ C_{-2}\\ C_{-1}\\ \\ \vdots\\ \\ C_{n-1} \end{bmatrix} \text{ and } \boldsymbol{F}=\begin{bmatrix} \alpha\\ F\\ \vdots\\ \\ \vdots\\ F\\ \beta \end{bmatrix},$$

and

$$\begin{aligned}\omega_1&=m(\varsigma_4)-b(\varsigma_3)+k(\varsigma_1),\\ \omega_2&=m(\varsigma_5)+k(\varsigma_2),\\ \omega_3&=m(\varsigma_4)+b(\varsigma_3)+k(\varsigma_1).\end{aligned}$$

By solving the matrix system, C is evaluated and substituted into Eq. (10) to obtain the approximate solution for Eq. (1).

3.3. Ode45

Ode45 is a build-in solver in MATLAB's standard solver for ordinary differential equations (ODEs). By using the same parameter as CTBS, Eq. (1) is also solved by using the following algorithm.

Algorithm 1

Algorithm 1. Code for solving Eq. (1) by using ode45

```
f = @(t,x) [x(2); (F-r*x(2)-k*x(1))/m];
tspan = t0:(0.05–0)/(n):tN;
ts = zeros(1,n); xs = zeros(1,n);
[ts,xs] = ode45(f,tspan,[0;0]);
```

4. Error analysis

The estimation of a truncation error for the proposed method is presented in this section. From approximate displacement in Eq. (14), the relationships can be obtained as follows:

$$h\left[x^{*\prime}(t_{j-1})+4x^{*\prime}(t_j)+x^{*\prime}(t_{j+1})\right]=3\left[x^{*\prime}(t_{j+1})-x^{*\prime}(t_{j-1})\right], \tag{17}$$

$$h^2x^{*\prime\prime}(t_j)=6\left[x^{*}(t_j)-x^{*}(t_{j+1})\right]-2h\left[x^{*\prime}(t_j)+x^{*\prime}(t_{j+1})\right], \tag{18}$$

$$h^3x^{*\prime\prime\prime}(t_{j+})=12\left[x^{*}(t_j)-x^{*}(t_{j+1})\right]+6h\left[x^{*\prime}(t_j)+x^{*\prime}(t_{j+1})\right], \tag{19}$$

$$h^3x^{*\prime\prime\prime}(t_{j-})=12\left[x^{*}(t_{j-1})-x^{*}(t_j)\right]+6h\left[x^{*\prime}(t_{j-1})+x^{*\prime}(t_j)\right]. \tag{20}$$

Then, $x^{*\prime\prime\prime}(t_{j+})$ and $x^{*\prime\prime\prime}(t_{j-})$ are the approximate values of $x^{*\prime\prime\prime}(t)$ in $[t_j, t_{j+1}]$ and $[t_{j-1}, t_j]$, respectively. By using the operator notation $E(x^{*}(t_j))=x^{*}(t_j)$, Eq. (17) can be written as

$$h(E^{-1}+4+E)x^{*\prime}(t_j)=3(E-E^{-1})x^{*}(t_j). \tag{21}$$

Since $E=e^{hD}$ where $D=\frac{d}{dx}$, operator E can be written in an expression form in powers of hD:

$$e^{hD}=1+hD+\frac{h^2D^2}{2!}+\frac{h^3D^3}{3!}+\frac{h^4D^4}{4!}+\frac{h^5D^5}{5!}+\cdots$$

$$e^{-hD}=1-hD+\frac{h^2D^2}{2!}-\frac{h^3D^3}{3!}+\frac{h^4D^4}{4!}-\frac{h^5D^5}{5!}+\cdots$$

Next, Eq. (21), can be written as

$$h(e^{-hD}+4+e^{hD})x^{*\prime}(t_j)=3(e^{hD}-e^{-hD})x^{*}(t_j). \tag{22}$$

Hence, can be given by

$$x^{*\prime}(t_j)=x^{*\prime}(t_j)-\frac{1}{180}h^4x^{*(5)}(t_j)+O(h^6). \tag{23}$$

By using the same approach for Eq. (17)-(20), we can derive the following relations:

$$x^{*\prime\prime}(t_j)=x^{*\prime\prime}(t_j)-\frac{1}{12}h^2x^{*(4)}(t_j)+\frac{1}{360}h^4x^{*(6)}(t_j)+O(h^6), \tag{24}$$

$$\begin{aligned}x^{*\prime\prime\prime}(t_{j+})=x^{*\prime\prime\prime}(t_j)&+\frac{1}{2}hx^{*(4)}(t_j)+\frac{1}{12}h^2x^{*(5)}(t_j)-\frac{1}{360}h^4x^{*(7)}(t_j)\\&-\frac{1}{1440}h^5x^{*(8)}(t_j)+O(h^6),\end{aligned} \tag{25}$$

$$\begin{aligned}x^{*\prime\prime\prime}(t_{j-})=x^{*\prime\prime\prime}(t_j)&-\frac{1}{2}hx^{*(4)}(t_j)+\frac{1}{12}h^2x^{*(5)}(t_j)-\frac{1}{360}h^4x^{*(7)}(t_j)\\&-\frac{1}{1440}h^5x^{*(8)}(t_j)+O(h^6).\end{aligned} \tag{26}$$

Then, Eq. (25)-(26) can be written as

$$\frac{1}{2}\left[x^{*\prime\prime\prime}(t_{j+})+x^{*\prime\prime\prime}(t_{j-})\right]=x^{*\prime\prime\prime}(t_j)+\frac{1}{12}h^2x^{*(5)}(t_j)+O(h^4) \tag{27}$$

and

$$x^{*\prime\prime\prime}(t_{j+})+x^{*\prime\prime\prime}(t_{j-})=hx^{*(4)}(t_j)-\frac{1}{720}h^5x^{*(8)}(t_j)+O(h^7). \tag{28}$$

Afterwards, $e(t)$ is defined as $e(t)=x^{*}(t_j)-x^{*}$ and the equations of (23)-(26) are substituted into $e(t_j+\theta h)$ to obtain

$$\begin{aligned}e(t_j&+\theta h)\\&=\frac{\theta^2(\theta-1)^2}{24}h^4x^{*(4)}(t_j)+\frac{\theta(\theta^2-1)(3\theta^2-2)}{360}h^5x^{*(5)}(t_j)+O(h^6).\end{aligned} \tag{29}$$

Subsequently, the cubic uniform trigonometry B-spline is $O(h^4)$ accurate.

5. Results and discussions

This section represented the approximate displacements generated by healthy and four pathological conditions of vocal cords, and then analysed accordingly. 100 recordings of each vocal cord condition which is healthy, hyperfunctional dysphonia (HD), laryngitis, functional dysphonia (FD) and recurrent laryngeal nerve paralysis (RLNP) were synthesized to obtained average of fundamental frequencies. Table 1 and Table 2 tabulated the parameters, and the average of fundamental frequencies for healthy and the pathological conditions of vocal cords. Three phases of phonation process will be considered; (i) early phase at 0.01 s, (ii) middle phase at 0.03 s and (iii) end phase at 0.05 s. The errors between CTBS and ode45 of each vocal cord condition will be evaluated as Error $=|x(t)-x^{*}(t)|$.

Fig. 1 illustrated the generated displacements of (a) healthy, (b) HD, (c) laryngitis, (d) FD and (e) RLNP. Numerically, the displacements and the errors of each condition obtained by comparing the approximate displacements between CTBS and ode45 are tabulated in Table 3 and 4. It can be seen that CTBS and ode45 has generated slightly equal

displacement within 0.05 s. The figure and numerical values revealed that CTBS is a reliable method in generating displacement of vocal cord when compared to ode45.

The phases of the phonation process of each vocal cord condition can be observed from Table 3. It is apparent from Table 3 that the value of displacements generated by healthy vocal cord steadily declined throughout the process. Nevertheless, the displacement of vocal cord with HD, laryngitis, FD and RLNP are fluctuated throughout the early, middle and end phases. The HD, laryngitis and RLNP condition have developed the fluctuation increase–decrease displacements while FD condition has formed decrease-increase displacements of phonation process.

Based on the trend which can be observed from Table 5, it can be assumed that healthy vocal cord has the widest opening at early phase of phonation process, which then decreased at the middle and more narrowed at the end phase. However, the fluctuated trend of the vocal cord with pathological conditions such as HD, laryngitis and RLNP have shown that they have wider opening at the middle phase than at the early phase. The opening of these vocal cords are then decreased at the end phase but still wider than at the early phase. Aside from that, vocal cord with FD has demonstrated a different fluctuation trend than other pathological condition. It can be deducted that vocal cord with FD's opening has decreased at the middle phase than at the early phase, but unexpectedly increased at the end phase.

6. Conclusion

In this work, the approximate displacements of five types of vocal cord conditions have been generated by using CTBS and ode45. Overall, it is evident that the generated approximate displacements by CTBS are approximately close to ode45. It can be concluded from the calculated error that CTBS is reliable method in generating displacements of vocal cord. The generated displacements also have been utilized to investigate the phases of phonation process. It can be pointed from the outcomes illustrated in Fig. 2 and Table 5, that healthy vocal cord presents the steadily decline phonation process. In contrast, another five pathological conditions have developed fluctuated displacement. Fluctuation of displacements value revealed the irregular displacements value generation that is a characteristic of pathological vocal cord (Bonilha and Deliyski, 2008) which caused by low stiffness. It may be the case therefore that vocal cord with pathological condition has lower stiffness than healthy vocal cord. Therefore, this work offers new insights into the speech production of healthy and pathological vocal cord through numerical results. Future researches are encouraged to investigate the effect of various pathological conditions towards the stiffness of vocal cord. This could aid in determining the relationship between vocal cord conditions towards its stiffness and the effect towards vocal cord displacements value.

CRediT authorship contribution statement

Nur Fatin Amirah Mohd Rodzi: Writing – original draft, Visualization, Software, Methodology, Investigation, Formal analysis, Data curation. **Shazalina Mat Zin:** Writing – review & editing, Project administration, Validation, Supervision, Resources, Data curation, Conceptualization. **Syatirah Mat Zin:** Formal analysis, Supervision, Validation, Visualization.

Declaration of competing interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

Acknowledgments

The authors would like to acknowledge the support from the Fundamental Research Grant Scheme (FRGS) under a grant number of FRGS/1/2019/STG06/UNIMAP/03/2 from the Ministry of Higher Education of Malaysia.

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