



# Modeling atmospheric emissions during olive husk drying and study of meteorological factors effect in the vicinity of urban areas

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## ABSTRACT

In this work, we present field measurement data and modeling of air pollutant during one season at an urban area in Sousse, east Tunisia. We analyzed the average pollutant emission and we used our data to evaluate a dispersion model. The impact of various meteorological factors on pollutants concentrations has been studied. The model predicts that the concentrations of CO and CO<sub>2</sub> in an urban area can reach 50 mg.m<sup>-3</sup> and 185 mg.m<sup>-3</sup> respectively. The height of the chimney, the wind velocity, the fuel nature, the air excess and the combustion temperature have an influence on the concentrations of pollutants and their dispersion.

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## 1. Introduction

Urban atmospheric pollution suggests an increasing concern because of its impact on the environmental (Clark et al., 2016) and public health (Lelieveld et al., 2015). Pursuit of development along the same industrial path that countries had been following for the last two centuries; Tunisia is currently expressing growth in air pollution. Atmospheric pollution becomes a real threat to human health (Rovira et al., 2015) mainly in the regions surrounds industrial sites. The dispersion of the particules pollutants contained in the exhaust gas from the stack is hugely depends on the landform and the environment around the pollution source. However, it is still unclear how these factors affect the dispersion of pollutants in industrial sites. Consequently, the study of the dispersion of pollutants within an industrial site becomes essential for the protection of human health in the regions of the site (Ma et al., 2017; Orru et al., 2015).

Meteorological factors affect the dispersion of pollutants. For example, wind speed can change the state of dispersion of the

atmosphere, while the wind direction creates a pathway for the transport of pollutants (Zeng and Zhang, 2017). Many studies have shown that low speed over a long period of time is the most important reason for heavy pollution processes (xu, 2005; Batterman et al., 2014).

Also, the stack effect has been widely studied (Yu et al., 2004; Jo et al., 2007; Lee et al., 2010) with the someproposed solutions. Many studies have been carried out to examine the stack effect on the fine induced smoke movement driven (Jaworski et al., 2014; Shi et al., 2014) and other studies focus on the influence of stack height on the distribution of pollutant concentrations in the neighborhood of the emitting building (Lateb et al., 2011).

Wind speed is also one of the factors affecting the dispersion of stack emissions. Indeed, the effect of wind speed on pollutant concentration is proportional to the increase of wind speed, (Wang and Ogawa, 2015; Duo et al., 2018).

Thus, the reduction of air pollution will have a positive impact on health, especially in densely populated areas. It is crucial to predict the concentrations for air quality management and study the wind flow variability between buildings which affects the dispersion mechanism.

Modeling of atmospheric dispersion is a significant tool for the response of fume emissions. This helps evaluating the impact consequences for the people exposed to the fume plume.

Several atmospheric dispersion models (ADM) for local scale and for range modeling has been developed (Conti et al., 2017). A recent comparison of various atmospheric dispersion models out-

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a gaz sample is analyzed. The temperature field, the [CO] and [CO<sub>2</sub>] were measured using a smoke analyzer (Testo 330-2LL) which provides data about each pollutant fraction. Experimental data provided by the smoke analyzer are recorded daily during the period 20 February–30 April 2012. Although, the smoke analyzer does not contain cells for detecting NO<sub>x</sub>, [CO] measurement remains important because compared to other pollutant rapidly dissociates (NO<sub>2</sub>) or quickly reacts with ozone (NO), has a long chemical lifetime (Connan et al., 2013). The measurement where illustrated in Table 1.

### 3. Atmospheric dispersion modeling

The Gaussian dispersion model assumed that the concentration of a pollutant in both the vertical and horizontal planes can be represented by a Gaussian distribution. According to the Gaussian model, the concentration in any point in 3D space is written in the following form

$$C(x, y, z) = \frac{q}{4 \times \pi \times u \times \sigma_y \times \sigma_z} \times \exp\left(-\frac{y^2}{2 \times \sigma_y^2}\right) \times \left(\exp\left(-\frac{(z-h)^2}{2 \times \sigma_z^2}\right) + \exp\left(-\frac{-(z-h)^2}{2 \times \sigma_z^2}\right)\right) \quad (1)$$

where C is the pollutant concentration (g·m<sup>-3</sup>), U represents the wind velocity (m·s<sup>-1</sup>), q is the pollutant mass flow rate (g·s<sup>-1</sup>), h denotes the chimney elevation (m) and  $\sigma_y$  and  $\sigma_z$  are the Gaussian standard deviations in the y and z direction.

Based on the Pasquill-Gifford stability class, the standard deviations  $\sigma_y$  and  $\sigma_z$  are calculated by the following formula (Pasquill, 1961).

$$\sigma_y^2 = \frac{2D_y x}{U} \quad (2)$$

and

$$\sigma_z^2 = \frac{2D_z x}{U} \quad (3)$$

$D_y$  and  $D_z$  are respectively the diffusion coefficients in the y and z direction and y is the distance from the source according to the y direction (km). These standard deviations are dependent on the length of the plume x-axis and on the meteorological condition. They are calculated based on the stability classification of the atmosphere (six categories (A-F)), where A corresponds to extremely unstable and F corresponds to very stable.

$$\sigma_y = ax^b \quad (4)$$

and

$$\sigma_z = cx^d + f \quad (5)$$

The constants a, b, c, d and f are functions of the stability conditions of the atmosphere. These coefficients depending on stability class and distance from the emission source (Turner, 1994).

**Table 1**

Data provided by the fume analyzer.

Test	DryingFlow	T <sub>A</sub> (C)	T <sub>F</sub> (C)	CO (%)	CO <sub>2</sub> (%)	O <sub>2</sub> (%)
1	low	34,6	74	3	0,4	20,5
2	Fort	34,8	71	3	2,8	17,4
3	low	34,9	74	3	0,4	20,5
4	Fort	34	69	0,6	2,1	18,1
5	Fort	28,2	87	0,3	3,1	17,8
6	Fort	24	69	0,6	2,1	18,1
7	Fort	23,7	90	0,19	2,31	18,5
8	Fort	27,5	104	0,27	2,6	18,9

T<sub>A</sub>: Ambient temperature, T<sub>F</sub>: Entry stacks gas temperature.

To search the concentration at ground level (z = 0) and knowing that the x-axis coincides with the axis panache, the Eq. (1) becomes (Cheng et al., 2015):

$$C(y) = \frac{q}{\pi \times u \times \sigma_y \times \sigma_z} \times \exp\left(-\frac{y^2}{2 \times \sigma_y^2}\right) \times \left(\exp\left(-\frac{h^2}{2 \times \sigma_z^2}\right)\right) \quad (6)$$

## 4. Results and discussions

### 4.1. Spatial variation of concentration

With the chimney height H of 5 m, which is the real height of the existing chimney and knowing that the two factory chimneys are of the same height and the same rate of smoke, we calculated the concentration of pollutant from two chimneys and the total concentration by superposition. Then a comparison is made between the values of the determined concentration and Tunisian ambient air (Table 2). Fig. 2 shows that the concentration of CO peaks at 50 μgm<sup>-3</sup> approximately 50 m of the source and decreases to zero value at 400 m. It shows that the concentration of CO<sub>2</sub> is rapidly increased to reach its maximum of 185 mgm<sup>-3</sup> at 50 m then decreases to a value of 30 mgm<sup>-3</sup>.

### 4.2. Factors influencing pollutant dispersion

#### 4.2.1. Effect of the stack height

To highlight the effect of the stackheight, we considered two sites with exactly the same conditions of temperature, pressure, flow, wind, and stack diameter, but different heights (5 m, 10 m, 30 m and 40 m), and the concentration variation as a function of x for the different heights are determined. We take the case where the velocity is equal to 4 m/s and the sun is strong and as a fuel anexhaustedolive husk.

Note that the concentrations of pollutants at ground level for H = 5 m are very high compared to the concentrations of pollutants from a stack with height H = 20 m (Fig. 3).

The study of this phenomenon is of great interest in terms of pollution, because it is obvious that the dispersion from a stack of low height will be quite different from that obtained with a tall stack, which will benefit from more favorable dispersion.

**Table 2**

National Ambient Air Quality Standards.

Pollutant	Type of average	Concentration limit value
CO	1 h	35 ppm (10 mg/m <sup>3</sup> )
NO <sub>2</sub>	1 h	0.350 ppm (660 μg/m <sup>3</sup> )
O <sub>3</sub>	1 h	0.12 ppm (235 μg/m <sup>3</sup> )
SO <sub>2</sub>	Annual arithmetic mean	0.03 ppm (80 μg/m <sup>3</sup> )
Pb	Annual arithmetic mean	2 μg/m <sup>3</sup>

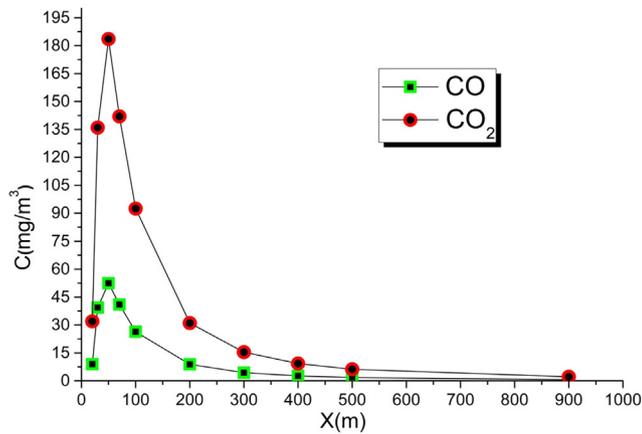


Fig. 2. Spatial evolution of [CO] and [CO<sub>2</sub>].

Thus, the use of tall stacks ensures good dispersion of gaseous pollutants, and leads to low concentrations of pollutants at ground level, but the solution to the pollution problem is not there,

because the impact is just not only at the source, but it spreads to great distances using meteorological factors (wind etc..).

4.2.2. Effect of wind speed

To mark the effect of wind speed on the pollutant dispersion, exhausted olive husk is used as a fuel, and then we determine the concentration evolution of pollutant according to the wind speed. We fixed the distance from chimney to 50 m and the chimney height is 5 m (Fig. 4).

There is a clear relationship between wind speed and the concentration levels of pollutants. Pollutant dispersion increases with wind speed and turbulence. A low wind therefore favors the accumulation of pollutants. When the wind speed is low, it can move away the pollutants with a certain zone, but, when the wind speed is high enough, it can carry a huge amount of pollutant from far away (wang and susuman, 2017). Indeed, when the wind speed increases, the dispersion, also, increases, and maximum concentrations go more away from the emission source. Dilution due to wind is even greater when the wind velocity is high. For a fixed rate of pollutants, the air rate, allowing dilution increases with velocity. In Fig. 4(a) at wind speed equal to 2 m/s and at moderate solar radiation, the diffusion is poor and is accompanied by a lower

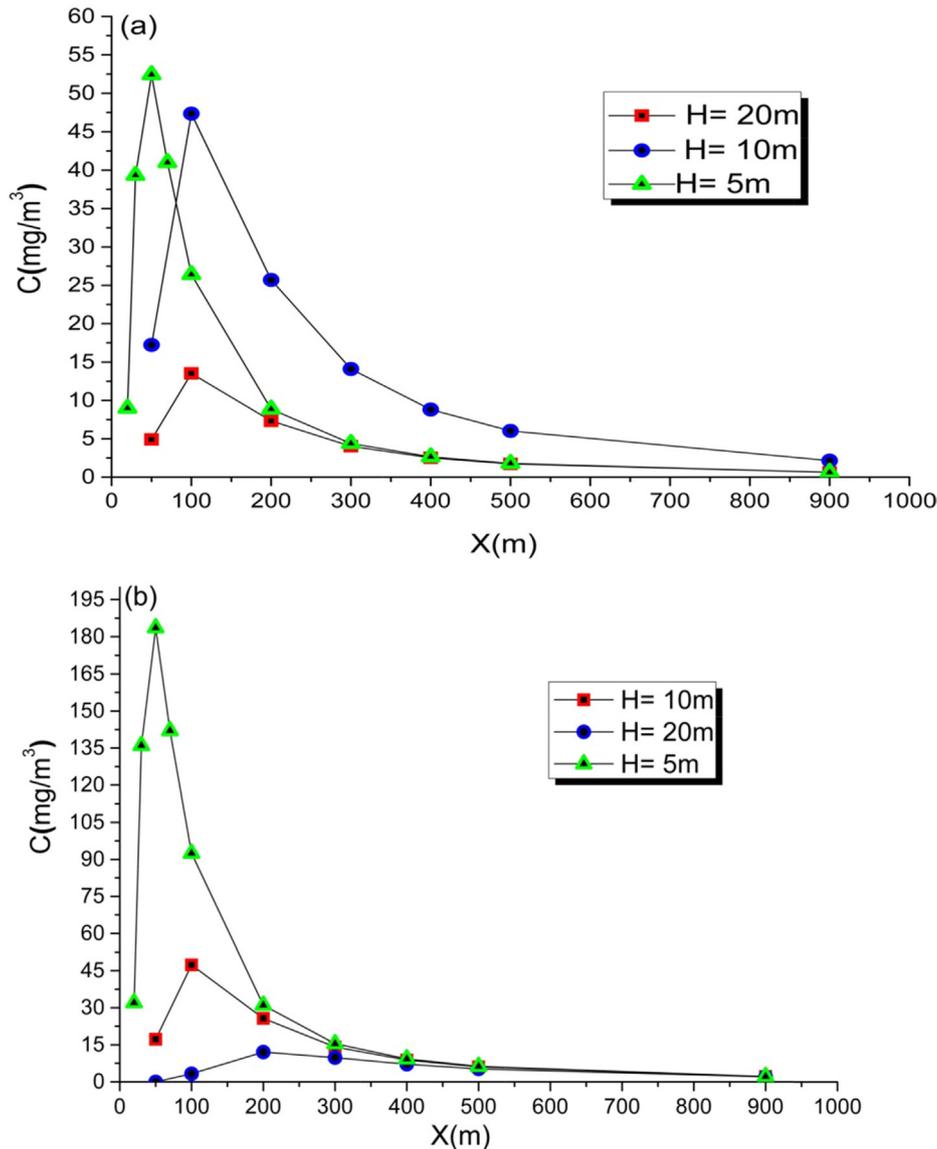


Fig. 3. Effect of stacks height on (a) CO and (b) CO<sub>2</sub> concentrations.

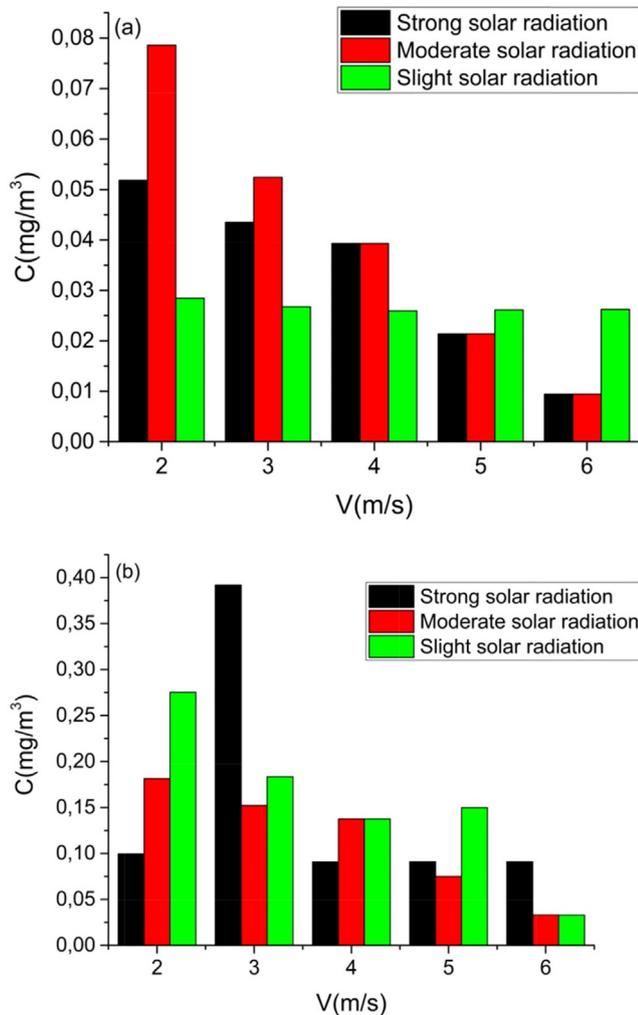


Fig. 4. Concentration versus wind speed for (a) CO and (b) CO<sub>2</sub> at different solar radiation.

Table 3  
Mass flow of various pollutants out of stacks (for natural gas).

Flow (Q)	CO	CO <sub>2</sub>	O <sub>2</sub>
Value (g/s)	5.46	57.53	6.86

atmospheric mixed layer, preventing the spread of pollutants and increasing the concentration (Zheng and yu, 2017).

#### 4.2.3. Effect of the fuel nature

We considered two sites with exactly the same conditions of temperature, pressure, flow, wind, and chimney diameter, but

Table 4  
Analytical measurements on natural gas combustion fumes.

No. Analysis:	A <sub>1</sub>	A <sub>2</sub>	A <sub>3</sub>	A <sub>4</sub>	A <sub>5</sub>	A <sub>6</sub>	A <sub>7</sub>	A <sub>8</sub>
Designation of analysis parameters	Values identified by calibrated combustion analyzer							
- Temperature of smoke (° C):	180.4	218	184.7	151.3	141.3	202.5	160.7	183.3
- - Ambient Temperature (° C):	22	22.3	21.9	22.8	23	25.9	27.1	24.3
O <sub>2</sub> (% Vol):	3.9	4.2	5.6	2.6	4.6	2.7	2.9	2.6
- CO <sub>2</sub> (% Vol):	9.61	9.38	8.64	10.34	9.22	10.28	10.17	10.34
CO (ppm):	91	57	64	0	0	11	12	0
- CO max (ppm):	253	64	66	1	2		34	47
- Losses (%):	7.5	9.5	5.6	5.8	5.8	8	6.1	7.1
- Yield (%):	92.5	90.5	94.4	94.2	94.2	92	93.9	92.9
λ	1.23	1.26	1.36	1.14	1.41	1.15	1.16	1.14
- Drawing down Chimney (mbar)	-0.03	-0.02	-0.03	-0.02	-0.02	-0.02	-0.02	

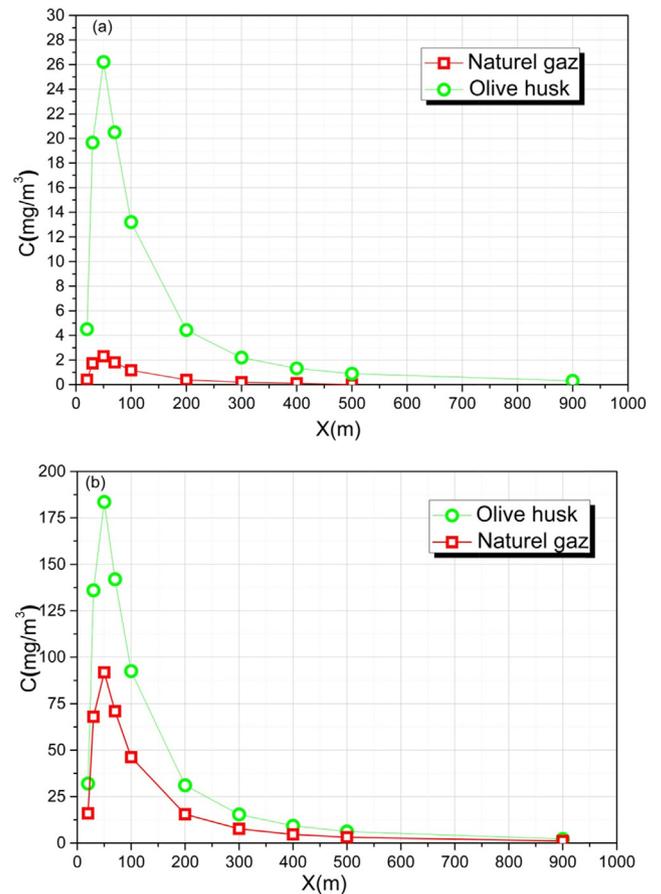


Fig. 5. Effect of fuel nature on (a) CO and (b) CO<sub>2</sub> concentrations.

using as a fuel exhausted olive husk and natural gas. We took the case where the velocity is equal to 6 m/s and the sun is strong, and we determined the concentration variation as a function of x to highlight the effect of the fuel type on pollutant dispersion. The flow rates of the different components of the smoke out of the chimney using as a fuel gas are given in Table 3 and the analytical measurements were provided in Table 4.

It is clear that the concentration of all pollutants produced by the combustion of exhausted olive husk is higher than that of these produced by the combustion of natural gas (Fig. 5). Using as a fuel exhausted olive husk, the [CO] increases until reaching its maximum at X = 50 m, then it starts to decrease away from the source. Similarly for natural gas, but the maximum of [CO] for this fuel is negligible compared to the use of exhausted olive husk. We can consider that natural gas is a clean gas generating little carbon dioxide and almost no other pollutants, since natural gas is mainly composed of methane (CH<sub>4</sub>) and therefore much more hydrogen than carbon. For this reason the rate of carbon dioxide (CO<sub>2</sub>) from

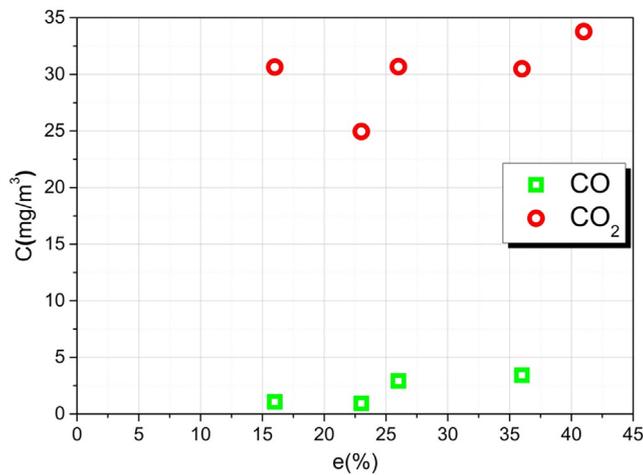


Fig. 6. Effect of excess air on CO and CO<sub>2</sub> concentrations.

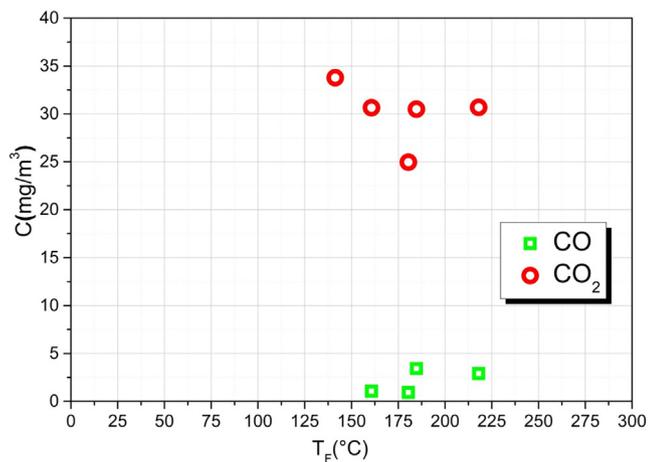


Fig. 7. Effect of the combustion temperature on CO and CO<sub>2</sub> concentrations.

the water produced by the hydrogen in the form of vapor (H<sub>2</sub>O) is less than that of other fuels. There is less carbon dioxide produced by caloric unit than other fuels.

#### 4.2.4. Effect of excess air

To determine the effect of the excess air in the dispersion of pollutants coming out of the chimney, the natural gas is used as a fuel, and varying the air flow entering the stove using a ventilator (Table 4). We took a wind velocity equal to 6 m/s, the sun is strong and X = 50 m. It is seen from Fig. 6 that CO decreases when the excess air increases, unlike CO<sub>2</sub> increases with air excess. Indeed, promoting excess air, it provides more CO and OH radicals, so the next reaction is stimulated:

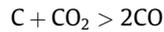
$\text{CO} + \text{OH} \rightarrow \text{CO}_2 + \text{H}^\bullet$ . So CO disappears in favor of CO<sub>2</sub>. Moreover, increasing the excess air decreases the temperature and consequently inhibits reactions:

- I)  $\text{CO}_2 + \text{C} \rightarrow 2\text{CO}$ : The reaction is promoted by raising the temperature and decreasing the pressure.
- II)  $\text{CO}_2 + \text{H}_2 \rightarrow \text{H}_2\text{O} + \text{CO}$ : It is also favored by increasing the temperature (but remains independent of pressure). Thus, the amount of CO released increases with the richness of the mixture.

#### 4.2.5. Effect of the combustion temperature

To determine the effect of the combustion temperature on pollutants dispersion leaving the chimney, natural gas is used as a fuel

and varying the air flow entering the stove using a fan. CO increases gradually as the temperature increases, unlike CO<sub>2</sub> that decreases when T increases this is done in the following reaction (Fig. 7).



## 5. Conclusion

In this work we evaluated first the pollutant concentration detected by the gas analyzer at ground level. The chimney height, the wind velocity, the solar radiation, the fuel nature, the air excess and the combustion temperature affects the pollutant dispersion. In fact, at wind speed equal to 2 m/s and at moderate solar radiation, the diffusion is poor and is accompanied by a lower atmospheric mixed layer, preventing the spread of pollutants and increasing the concentration.

The use of tall stacks ensures good dispersion of gaseous pollutants, and leads to low concentrations of pollutants at ground but the solution to the pollution problem is not there, because the impact is just not only at the source, but it spreads to great distances through meteorological factors.

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